Interaction among autoregulation, CO₂ reactivity, and intracranial pressure: a mathematical model

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Ursino, Mauro, and Carlo Alberto Lodi. Interaction among autoregulation, CO₂ reactivity, and intracranial pressure: a mathematical model. Am. J. Physiol. 274 (Heart Circ. Physiol. 43): H1715–H1728, 1998.—The relationships among cerebral blood flow, cerebral blood volume, intracranial pressure (ICP), and the action of cerebrovascular regulatory mechanisms (autoregulation and CO₂ reactivity) were investigated by means of a mathematical model. The model incorporates the cerebrospinal fluid (CSF) circulation, the intracranial pressure-volume relationship, and cerebral hemodynamics. The latter is based on the following main assumptions: the middle cerebral arteries behave passively following transmural pressure changes; the pial arterial circulation includes two segments (large and small pial arteries) subject to different autoregulation mechanisms; and the venous cerebrovascular bed behaves as a Starling resistor. A new aspect of the model exists in the description of CO₂ reactivity in the pial arterial circulation and in the analysis of its nonlinear interaction with autoregulation. Simulation results, obtained at constant ICP using various combinations of mean arterial pressure and CO₂ pressure, substantially support data on cerebral blood flow and velocity reported in the physiological literature concerning both the separate effects of CO₂ and autoregulation and their nonlinear interaction. Simulations performed in dynamic conditions with varying ICP underline the existence of a significant correlation between ICP dynamics and cerebral hemodynamics in response to CO₂ changes. This correlation may significantly increase in pathological subjects with poor intracranial compliance and reduced CSF outflow. In perspective, the model can be used to study ICP and blood velocity time patterns in neurosurgical patients in order to gain a deeper insight into the pathophysiological mechanisms leading to intracranial hypertension and secondary brain damage.

intracranial hemodynamics; cerebral blood flow; cerebral blood volume; cerebrovascular control mechanisms

The cerebrovascular bed in humans and animals is subjected to the action of sophisticated regulatory mechanisms that work to maintain an adequate cerebral blood flow (CBF) for functional and metabolic needs. Intracranial vessels respond promptly to changes in cerebral perfusion pressure (CPP; cerebral arterial pressure minus cerebral venous pressure); the response, called autoregulation, ensures that CBF remains approximately constant in the CPP range of 50–150 mmHg (38). Moreover, cerebral vasculature is particularly sensitive to chemical stimuli, especially O₂ and CO₂ tension in arterial blood. These mechanisms interact in complex nonlinear ways in response to perturbations affecting pressure and blood concentration levels simultaneously.

There are many factors that make the analysis of cerebrovascular regulation particularly complicated. First, consecutive vascular segments in the brain contribute differently to CBF control, a phenomenon often referred to as “segmental heterogeneity” (6). Some authors have observed that the large pial vessels play a major role in the regulatory response to moderate arterial pressure changes, whereas small pial arteries undergo massive vasodilation when CPP approaches the lower autoregulation limit (25, 29).

In addition, cerebral circulation takes place within a closed space (the skull and the craniospinal axis) with only a limited capacity to buffer blood volume changes; consequently, any modification in vessel caliper (either passive or induced by cerebrovascular regulatory mechanisms) may affect intracranial pressure (ICP) through changes in cerebral blood volume (CBV). Because ICP is the extravascular pressure of cerebral vessels and is almost equal to pressure in the large cerebral veins, its changes can have a significant impact on cerebral hemodynamics.

Because of the close relationship among the action of cerebrovascular control mechanisms, CBV, and ICP, CBF can be affected by several noncirculatory aspects of intracranial dynamics, especially craniospinal elasticity (defined by the intracranial pressure-volume relationship) and the circulation of cerebrospinal fluid (CSF).

The interaction among ICP, CBV, and cerebrovascular regulation must be taken into account in the treatment of patients with severe brain lesions. Changes in arterial CO₂ pressure (PacO₂) and mean systemic arterial pressure (SAP) are frequently used in neurosurgical intensive care units to assess the status of cerebrovascular control mechanisms (8, 48). Moreover, manipulation of arterial CO₂ concentration is routinely used as a therapeutic means in controlling ICP and adjusting CBF to metabolic requirements (34, 37). However, uncontrolled changes in CO₂ or in arterial pressure can have a dramatic impact on ICP and CBF, leading to acute intracranial hypertension and cerebral ischemia (12).

The complexity of the aforementioned relationships makes it difficult to achieve a clear understanding of cerebrovascular control in simple qualitative terms. For this reason, various mathematical models of cerebral hemodynamics and ICP dynamics have been presented in past years (7, 21, 22, 31, 47, 49). We recently developed a mathematical model of the interaction among cerebral autoregulation, CBV changes, and ICP in humans (50, 51). The model was able to reproduce various phenomena concerning ICP, such as the genesis of plateau waves (51), the ICP response to arterial pressure perturbations (14), or the ICP changes in-
duced by bolus injection within the craniospinal space (PVI tests) (52).

The aim of this study was to significantly improve and extend the previous model to include the CO2 reactivity of cerebral vessels, its nonlinear interaction with ICP and with cerebral autoregulation, and the description of the transcranial Doppler (TCD) velocity signal. The TCD technique, in fact, is routinely used today to assess cerebral hemodynamics due to its characteristics of noninvasiveness and continuous data acquisition (1).

There are two main justifications for developing this new model. We aimed to 1) demonstrate that several experimental results on cerebral autoregulation and chemical CBF regulation presented in past years can be summarized into a single theoretical setting, and 2) improve the interpretation of clinical maneuvers concerning cerebrovascular control and ICP dynamics.

The present preliminary study presents the model, its justification on the basis of current physiological knowledge, and its validation through experimental results taken from physiological literature. A second, related study (27) presents a sensitivity analysis of model parameters and validation of the model on the basis of clinical data from real patients with severe head trauma.

**QUALITATIVE MODEL DESCRIPTION**

The model is qualitatively presented, with attention focused on its new aspects. A more thorough analysis can be found in previous reports (50, 51). The complete set of mathematical equations is given in the APPENDIX.

**Intracranial Hemodynamics and CSF Dynamics**

The main biomechanical law at the basis of intracranial dynamics is the constancy of the overall volume contained in the craniospinal space. This principle, known as the Monro-Kellie doctrine, implies that any volume variation in an intracranial compartment causes a compression or dislocation of the remaining volumes, accompanied by an alteration in ICP. This phenomenon is mathematically reproduced by means of intracranial compliance (Cic), which represents the capacity of the craniospinal system to store a volume load. We assumed that this quantity is inversely proportional to intracranial pressure (Pic) through a constant parameter called the elastance coefficient (ke) (5, 31).

\[
C_{ic} = \frac{1}{k_e \cdot P_{ic}}
\]

In the present model, volume changes in the intracranial cavity are ascribed to four compartments: large pial artery volume (V1), small pial artery volume (V2), cerebral venous volume (Vv), and CSF volume (VCFS). The following volume preservation equation holds

\[
C_{ic} \frac{dP_{ic}}{dt} = \frac{1}{k_e \cdot P_{ic}} \left( \frac{dP_{ic}}{dt} \right) = \frac{dV_1}{dt} + \frac{dV_2}{dt} + \frac{dV_v}{dt} + \frac{dV_{CSF}}{dt}
\]

where t is time.

The electric analog in Fig. 1 represents the four intracranial compartments considered in the model and their mutual relationships, together with the extracranial venous drainage pathway. These are briefly described in the following sections.

Pial arteries and arterioles. Pial arteries and arterioles comprise the sections of the cerebrovascular bed directly under the control of regulatory mechanisms. We make a distinction between two consecutive segments, the large pial arteries (proximal segment) and the medium and small pial arteries (distal segment). In the following equation, subscript j = 1 indicates a quantity or a parameter that belongs to the proximal arteries, whereas subscript j = 2 refers to the distal arteries. Each segment is represented by a transverse hydraulic capacity (Cj), at which all blood volume changes are concentrated, and a longitudinal hydraulic conductance (Gj), which reproduces the pressure drop upstream and downstream of the capacity. The distinction between two segments is justified by the heterogeneity of cerebrovascular regulation (6).

Conductance and blood volume changes are calculated by simulating each segment as the parallel arrangement of several vessels with equal radius. Blood volumes are proportional to the second power of the inner radius, whereas conductances are proportional to the fourth power of the inner radius, according to the Hagen-Poiseuille law (33). This representation does not aim at reproducing the actual anatomic configuration of the cerebrovascular bed; rather, it aims to describe how a certain variation of vessel caliper, induced by cerebral autoregulation and/or CO2 reactivity, can influence vascular resistance and blood volume in a given segment.

A value for the inner radius (rj) is computed starting from the equilibrium of forces acting on the wall of the vessel, supposedly cylindrical (Laplace law)

\[
P_{ij} - P_{le}(r_j + h_j) = T_{e,j} + T_{m,j} + T_{v,j} \quad j = 1, 2
\]

where Pj is the intravascular pressure in the jth segment; Pic is the extravascular (i.e., intracranial) pressure; hj is wall thickness; and Te,j, Tm,j, and Tv,j denote elastic, smooth muscle, and viscous tensions, respectively.

Wall thickness is calculated as a function of inner radius, assuming that the vessel wall is incompressible; hence, its volume remains constant. Mathematical expressions for tensions have been given to reproduce results of experimental studies on isolated arterioles (10).

Examples of the tension-inner radius diagrams at steady-state conditions for proximal and distal pial arteries are shown in Fig. 2. The equilibrium points can be located on the curve for different working conditions. It can be seen that the percentage of radius change during maximal vasodilation is greater in the small pial arteries than in proximal arteries, in accordance with results of physiological experiments (6, 25, 29, 32, 53).

The geometric parameters characterizing the large and small pial arteries (i.e., inner radii in unstrained conditions and in basal conditions, thickness-to-radius ratio, and overall blood volume in basal conditions) have been set according to data reported previously (50, 51). The only difference is that, in the present model, the inner radius in the first segment is 10 times smaller than in previous studies. In fact, in earlier versions of the model, the first segment was representative not only of large pial vessels but also of basal cerebral arteries, both of which were assumed to be actively regulated by a pressure-dependent autoregulation mechanism (32). In this new model, however, with reference to more recent data (13, 36), we have assumed that the large basal arteries in the circle of Willis are not directly involved in the cerebral autoregulation response. Large basal arteries have therefore been treated as purely passive in nature.
The values of conductances in basal conditions have been assigned to reproduce a typical pressure distribution in the pial circulation as reported previously (50, 51). Cerebral venous circulation. The circulatory pathway from cerebral capillaries down to the dural sinuses also consists of a series arrangement of venous capacity and upstream and downstream longitudinal conductances. Because autoregulation plays a negligible role in cerebral veins (4), we adopted a simpler description for venous mechanics than for the pial arterial-arteriolar vasculature. The venous compliance ($C_{vi}$) is inversely dependent on the local transmural pressure, implying a monoexponential pressure-volume relationship. The terminal portion of the intracranial venous bed (bridge veins and lateral lacunae or lakes, represented by the conductance $G_{vs}$ in the model) passively collapses or narrows during intracranial hypertension, with a mechanism similar to that of a Starling resistor (4, 33). Because of this mechanism, cerebral venous pressure ($P_{v}$) is always slightly higher than ICP, and upstream large cerebral veins and venules remain open during intracranial hypertension. Consequently, conductance of the proximal venous circulation ($G_{pv}$) is constant. The remaining part of the vascular bed, from dural sinuses down to the heart, is summarized by the hydraulic conductance ($G_{ve}$) and compliance ($C_{ve}$) of the extracranial venous pathways.

CSF compartment. We have assumed that the processes of both CSF production at the cerebral capillaries and CSF outflow at the dural sinuses are passive and unidirectional. Hence, they are proportional to the corresponding transmural pressure value and fall to zero when this becomes negative. All the parameters that describe the venous and CSF compartments have been given the same basal values used in previous studies, for which thorough discussions of these quantities can be found (50, 51).

Middle cerebral artery blood flow velocity. Additional equations in the model have been included to estimate an approximate value for blood flow velocity in the middle cerebral artery (MCA) and to compare it with experimental data as recorded with the TCD technique. On the basis of studies conducted on healthy subjects and neurosurgical patients (13, 36), we assumed that the behavior of the MCA is essentially passive in nature; the transmural pressure ($SAP - ICP$) is a monoexponential function of the inner radius (Fig. 3). The parameters of this relationship have been set to reproduce the pressure-radius curves concerning human intracranial basal arteries (20). Finally, the MCA velocity ($V_{MCA}$) is calculated as the ratio of blood flow to vessel cross-sectional area. To this end, we assumed that about one-third of total CBF passes through each MCA. Based on these assumptions, the basal value of $V_{MCA}$ in the model is as high as 60 cm/s, which agrees with the values reported by Aaslid et al. (1).
Cerebrovascular Regulation Mechanisms

Cerebrovascular regulation mechanisms act on smooth muscle tension of large pial arteries and arterioles. To reproduce their action, we assumed that the amplitude of the "active tension-inner radius" relationship ($T_{\text{max},j}$) depends on an activation factor ($M_j$) that represents the degree of smooth muscle contraction in the given segment. Hence

$$T_{\text{max},j} = T_{\text{max}0,j}(1 + M_j)$$

where $T_{\text{max}0,j}$ is a constant parameter. The value $M_j = 0$ indicates basal conditions. When $M_j > 0$, there is active vasoconstriction, whereas $M_j < 0$ is associated with a condition of cerebral muscle relaxation and vasodilation.

The block diagram in Fig. 4 shows how feedback mechanisms modulate the activation factor. The upper branch refers to cerebrovascular autoregulation mechanisms, whereas the lower branch refers to CO2 reactivity. The contributions of autoregulation and CO2 reactivity to smooth muscle tension in the $j$th segment are described by two state variables, $X_{\text{aut},j}$ and $X_{\text{CO2},j}$, respectively. The dynamics of each is reproduced by means of a first-order low-pass filter, characterized by a gain factor ($G_{\text{aut},j}$ or $G_{\text{CO2},j}$) and a time constant ($\tau_{\text{aut},j}$ or $\tau_{\text{CO2},j}$).

As shown in Fig. 4, we have assumed that autoregulation acts on large pial arteries and small arterioles by means of two distinct feedback mechanisms: the mechanism on large arteries depends on changes in CPP, reflecting a myogenic or neurogenic mechanism; and the mechanism on small arteries is triggered by alterations in blood flow to cerebral tissue, according to a metabolic or endothelium-dependent response. This distinction aims at reproducing the heterogeneity of autoregulation observed by Kontos et al. (25) and MacKenzie et al. (29) in cats.

In contrast, CO2 is assumed to affect smooth muscle tension, in both large and small pial arteries, through a similar mechanism. Because the prevalent hypothesis attributes the vasoactive effect of CO2 to pH changes in the perivascular space (24, 34), we have assumed that model response depends on the logarithm of CO2 changes rather than on $P_{CO2}$ by itself. Hence, the following input quantity is used in the block diagram in Fig. 4

$$\Delta P_{\text{CO2}} = \log_{10} \frac{P_{\text{CO2}}}{P_{\text{CO2}0}}$$

The parameter $P_{\text{CO2}0}$ denotes the level of CO2 pressure that does not affect the basal smooth muscle tension. By changing this parameter, adaptation of cerebrovascular reactivity to prolonged hypercapnia or hypocapnia can be simulated (34, 39).

Furthermore, we have included two kinds of nonlinear interaction between autoregulation and CO2 reactivity. First, on the basis of several experimental studies (8, 18), we have assumed that the strength of the CO2 mechanism is not independent on CPP but, rather, is attenuated during severe brain ischemia. Ischemia, in fact, causes tissue acidosis, which has a buffering effect on the influence of CO2 on cerebral pH. Accordingly, the CO2 reactivity in the model decreases exponentially when CPP falls below normal (see inset in Fig. 4).

Second, Fig. 4 shows that autoregulation and CO2 reactivity are not simply summed to obtain the activation factor ($M_j$);
rather, they interact through a sigmoidal relationship, which accounts for the existence of lower and upper limits for cerebrovascular reactivity.

A value characterizing the parameters in the sigmoidal relationship has been set so that smooth muscle tension falls to zero during maximal vasodilatation and can rise to twice the basal value during maximum vasoconstriction.

The autoregulation time constants were set at the same values used in previous studies (50, 51). In particular, we assumed that the pressure-dependent mechanisms acting on large pial arteries exhibit rapid dynamics ($\tau_{aut,1} = 10$ s), whereas the flow-dependent response of pial arterioles is slightly slower ($\tau_{aut,2} = 20$ s).

The choice of time constants for CO$_2$ reactivity deserves further comment. Kontos et al. (24) found that arteriolar dilation in response to a pH decrease takes place rapidly, with a time constant of <10 s. Schneider et al. (43), during experiments on feline pial arteries with the use of a microelectrode, observed that pH and vascular diameter varied with a delay of ~30 and 45 s, respectively, after a CO$_2$ change. Severinghaus and Lassen (45) reported a time constant of 20 s. Schneider et al. (43), during experiments on feline pial arteries with the use of a microelectrode, observed that pH and vascular diameter varied with a delay of 7 and 48 s. It is worth noting that, in the last three cases, the measured quantity was the end-tidal CO$_2$ pressure; the observed delays therefore also included the transit time for blood to pass from the lung to the brain. Because in our model the input quantity is the arterial CO$_2$ pressure, the time constant includes only the time necessary for PaCO$_2$ to alter perivascular pH and that required for the vessel to react to a pH change. Hence, we have chosen a value of $\tau_{CO_2,j} = 20$ s for both large and small pial arteries. In the analysis of neurosurgical patients reported in our related paper (27), we have used a greater value for the parameter $\tau_{CO_2,j}$, because the monitored quantity is end-tidal rather than arterial CO$_2$ pressure.

Values for the gain factors of regulation mechanisms have been set to reproduce results obtained in animals when experiments are executed at constant ICP (see RESULTS).

A list of all model parameters and their values at basal conditions can be found in Table 1.

### RESULTS

Model simulations have been performed to analyze 1) cerebral autoregulation, 2) CO$_2$ reactivity, 3) the interactions between these two mechanisms, and 4) the effect of acute changes in CO$_2$ on ICP. With regard to the first three topics, only results obtained under steady-state conditions are presented and compared with experimental data. Moreover, to simulate experiments performed with the dura opened or at constant ICP, during these trials we used an extremely low value for the intracranial elastance coefficient. Hence, ICP changes were negligible throughout the simulations (ICP = 9.5 mmHg). In contrast, the last trials concern dynamic conditions, with ICP free to change as a consequence of blood volume and CSF volume alterations.

### Cerebral Autoregulation

Figure 5 shows the percent changes in inner radii in large and small pial arteries, percent change in CBF, and percent change in V$_{MCA}$ evaluated under steady-state conditions at different values of mean SAP. A value was applied to the parameters that describes the autoregulation gain in both segments (i.e., $G_{aut,i}$ in Fig. 4 and Eqs. 23A and 24A in APPENDIX) to reproduce the inner radius percent changes measured by Kontos et al. (25) and MacKenzie et al. (29) on animals; the correspondence is quite good. The results show that the importance of each pial segment depends on the arterial pressure level. During moderate SAP alterations, the changes in vessel caliber are more pronounced in the large pial arteries than in the arterioles. When arterial pressure is further decreased and approaches the autoregulation lower limit, dilation of small pial arteries becomes progressively greater, causing an enlargement of the cerebrovascular volume, whereas the response of

### Table 1. Values of model parameters in basal conditions

<table>
<thead>
<tr>
<th>Parameter Values</th>
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<tr>
<td>$f_{MCA} = 0.15$ cm</td>
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<tr>
<td>$f_{MCA} = 0.0075$ cm</td>
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<tr>
<td>$G_{aut,1} = 0.020$ mmHg$^{-1}$</td>
</tr>
<tr>
<td>$G_{CO_2,1} = 20$ s</td>
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<tr>
<td>$K_{m,1} = 1.02$</td>
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<tr>
<td>$t_{aut,1} = 10$ s</td>
</tr>
<tr>
<td>$G_{CO_2,1} = 154.32$ mmHg$^{-1}$</td>
</tr>
<tr>
<td>$G_{CO_2,1} = 4.64$</td>
</tr>
<tr>
<td>$K_{CO_2} = 20$</td>
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<tr>
<td>$b_{CO_2} = 0.65$</td>
</tr>
<tr>
<td>$\rho_{an} = 100$ mmHg$^{-1}$</td>
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<tr>
<td>$q_{p} = 12.5$</td>
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<tr>
<td>$P_{IC} = 9.5$ mmHg</td>
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<tr>
<td>$P_{CO_2,n} = 40$ mmHg</td>
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Subscripts 1 and 2 in paired parameters refer to large pial arteries (proximal segment) and small pial arteries (distal segment) of cerebrovascular bed. Refer to text for parameter definitions.
the larger vessels is rapidly exhausted. At very low or very high values of mean SAP, the inner radii behave in a completely passive way. The simulated pattern of CBF and $V_{MCA}$ versus mean SAP also agrees with that of experimental data (19, 29, 35). Autoregulation is able to maintain a fairly constant CBF in the range of 50–150 mmHg (38); $V_{MCA}$ does not decrease because of the passive variation in cross-sectional area (see Eq. 21A in APPENDIX). This result agrees with Nelson et al. (35), who found that velocity is always higher than CBF. Beyond the lower limit of autoregulation, CBF and $V_{MCA}$ start to decrease, despite the evident vasodilation of the small pial arteries.

**CO$_2$ Reactivity**

Figure 6 shows the dependence of inner radii, CBF, and $V_{MCA}$ on Pa$_{CO_2}$ under steady-state conditions. The value indicating normocapnia has been fixed at Pa$_{CO_2} = 40$ mmHg. Also in this case, a value for the gain factors describing CO$_2$ reactivity (i.e., $G_{CO_2}$) in Fig. 4 and Eq. 25A in APPENDIX) was set to reproduce the inner radius percent changes observed during experiments on animals. The comparison between simulation results and the corresponding experimental and clinical data proves to be suitable (18, 26, 30, 40, 41, 44, 53). Also in this condition, as during autoregulation, the amount of vessel variation is more pronounced in the small pial arteries than in the large pial arteries. This finding agrees with the observation made by Wei et al. (53), who demonstrated that the CO$_2$ reactivity in the arterioles of cats is dependent on vessel size. Moreover, the vasoconstrictive effect of hypocapnia reduces CBF to one-half its normal value. During hypercapnia, vasodilation can even double CBF. $V_{MCA}$ percent changes closely resemble those in CBF.

**Interaction Between Autoregulation and CO$_2$ Reactivity**

Figure 7 (bottom) shows the percent changes in small pial artery radius induced by arterial hypotension during normocapnia and hypercapnia. Figure 7 (top) displays the difference between vessel diameters during normocapnia and hypercapnia, which is considered an index of the CO$_2$ reactivity at different arterial pressure levels. As the model (Fig. 7, left) clearly shows, CO$_2$ reactivity initially increases with lowering mean SAP; afterward, when vasodilation in the small pial vessels becomes appreciable, CO$_2$ reactivity rapidly decreases. These findings qualitatively concur with the data reported by Wei et al. (53) (Fig. 7, right). The behavior shown in Fig. 7 can be attributed to the presence of nonlinear sigmoidal interaction between the two mechanisms that reflects the existence of upper and lower saturation levels for smooth muscle tension (see block diagram in Fig. 4).

Figure 8 describes the dependence of CBF on mean SAP (autoregulation curve) under steady-state conditions at various Pa$_{CO_2}$ levels. Obviously, an increase in Pa$_{CO_2}$ causes an increase in CBF at a given arterial pressure value. At the same time, the lower autoregulation limit shifts toward higher pressure; in fact, cerebral vessels are nearly maximally dilated because of hypercapnia and therefore are unable to dilate further in response to arterial hypotension. These findings are confirmed by several authors who studied the effects of induced hypotension at various Pa$_{CO_2}$ levels (16, 17, 37, 39).

Figure 9 describes the effect of arterial hypotension on the relationship between CBF and Pa$_{CO_2}$. Model results are compared with those obtained by Harper
and Glass (18) during experiments on dogs. It can be seen that arterial hypotension progressively reduces CO₂ reactivity. The most considerable effect of hypotension is visible during hypercapnia, when the arterial bed is already dilated to the maximum. On the other hand, experimental data suggest that the vasoconstrictory effect of hypocapnia is also reduced during severe hypotension (18). The model can reproduce this behavior, attributing it to a reduction in the CO₂ reactivity during cerebral ischemia (see block diagram in Fig. 4 and Eqs. 25A and 26A in APPENDIX).

Effects of Hypocapnia and Hypercapnia on ICP

The purpose of the following simulations, performed with ICP free to change, is to analyze the possible effects of CO₂ variations on ICP in patients with head injuries. This matter has been analyzed in depth in a second, related paper (27). We shall consider a hypothetical patient with moderate increase in CSF outflow resistance, hence with moderate intracranial hypertension. Three different cases, characterized by a progressive reduction in craniospinal elasticity, are presented.

Figure 10 shows the ICP response to an acute rise in PaCO₂. Hypercapnia causes a vasodilation with an increase in CBV, leading to a sudden ICP rise; subse-
of intracranial dynamics is an essential prerequisite in the treatment of severe brain diseases.

An important methodological aspect of this study is that many different experimental results, concerning various phenomena of intracranial dynamics often considered separately in the literature, can be summarized into a single theoretical setting. The main aspects elucidated in this work are discussed separately below.

**Cerebrovascular Segmental Heterogeneity**

A critical choice in the model concerns the subdivision of the cerebrovascular bed into several consecutive segments, each characterized by its own parameters and a specific functional response to pressure and/or CO₂ changes. Our segmentation largely concurs with that proposed by Kontos and colleagues (25, 53); these authors observed a vessel-size dependence in the response to blood pressure and CO₂ changes between small and large pial arteries. This different behavior of the pial vascular bed, confirmed in other studies (29, 32), is shown by our model to be a mere consequence of the Laplace law and of the different values of intravascular pressure at consecutive levels of the pial vasculature.

Moreover, in this study, as in a previous one (51), we assumed that autoregulation of the large pial artery is dominated by pressure-dependent mechanisms, whereas the response of small pial arteries mainly depends on blood flow changes. This hypothesis permitted us to reproduce not only the active response of the vessels quite well but also all CBF and V<sub>MCA</sub> changes at many levels of arterial pressure and CO₂. Hence, we are confident that this subdivision into two regulated seg-

**DISCUSSION**

The present work improves our previous model significantly, including the analysis of CO₂ cerebrovascular reactivity and the interaction among CO₂, autoregulation, and ICP. The model aims at representing an acceptable compromise between physiological accuracy and clinical usefulness. In fact, even though the emphasis of this study is on the modeling of physiological experiments, an understanding of the pathophysiology
CO2 reactivity is quantified by an index equal to CBF cerebral vessel vasomotor capacity (8, 12, 48). Usually conducted on neurosurgical patients to assess capnia and hypocapnia (18, 26, 30, 35, 40, 41, 44, 53). With regard to human subjects, Tenjin et al. (48) suggested the value 2.0%/mmHg as a threshold to discriminate between patients with preserved and impaired CO2 reactivity.

Interaction Between Autoregulation and CO2 Response

An important aspect of CBF control, documented in many physiological and clinical studies, is the presence of a significant nonlinear interaction between CO2 reactivity and autoregulation. Simulating the nature of this interaction is not only a problem of physiological importance but also is one that may have a great clinical impact. First, it is generally accepted that CO2 reactivity is an important prognostic index significantly correlated with clinical outcome. Nevertheless, knowledge of this index alone may be misleading if not integrated with information on arterial pressure, CBF, and autoregulation status. Second, hyperventilation is an effective means routinely used to control ICP in neurosurgical patients. However, the effectiveness of this maneuver hinges on mean SAP and autoregulation, a fact that should be kept in mind by clinicians when planning patient treatment (12). Finally, anyone trying to identify the parameters characterizing CBF control (e.g., the gains and time constants of the mechanisms) needs to consider their complex interactions and nonlinear “inhibitory-facilitatory” summation. The latter problem is addressed in the second, related paper (27).

Several experimental results show that arterial hypotension can critically interfere with the cerebrovascular response to CO2 changes. Harper and Glass (18), in a classic study, demonstrated that reducing arterial pressure to about one-third that of normal completely eliminates the vasodilatory response to hypercapnia and seriously weakens the vasoconstrictory response to hypocapnia. The latter result was further confirmed by others (2, 3).

A thorough analysis of the interaction between autoregulation and hypercapnia on pial vessel response can be found in the study by Wei et al. (53). According to their findings (see Fig. 7), the interaction between the two mechanisms is significantly nonlinear, i.e., the superimposition of the effects does not hold. In particular, as blood pressure decreases starting from a basal level, the responsiveness to CO2 becomes initially greater, suggesting a “facilitatory” overlapping of the two mechanisms. However, when arterial pressure approaches the autoregulation lower limit, CO2 responsiveness progressively disappears, indicating an “inhibitory” overlapping of autoregulation and hypercapnia.

It is well known that hypercapnia and hypocapnia significantly modulate the autoregulation curve. Hyper-
capnia shifts the autoregulation plateau to higher CBF levels, and hypocapnia reduces it to a lower CBF. Moreover, data collected by several authors concur, showing that the lower autoregulation limit is fairly shifted by CO2 changes (16, 17, 37, 39). More controversial results can be found for the effect of CO2 on the upper limit of autoregulation (11, 16, 38).

We were able to qualitatively reproduce most of the results mentioned above (Figs. 7–9) by supposing the presence of only two significant nonlinearities in the interaction between autoregulation and CO2 response. Both nonlinearities are confirmed by physiological considerations.

A first nonlinearity in the model derives from a sigmoidal static relationship and accounts for the natural bounds of smooth muscle tension (see last block in Fig. 4) and permits reproduction of most of the nonlinearities observed during combined stimuli. However, the presence of this sigmoidal relationship for smooth muscle tension did not allow us to explain the lack of vasoconstrictory response to hypocapnia observed during severe arterial hypotension (2, 3, 18). It has been claimed that the failure of cerebral vessels to constrict to hypocapnia during hypotension indicates that maintenance of adequate tissue O2 supply prevails over the maintenance of adequate CO2 and acid-base levels (18).

To account for this phenomenon, we assumed that cerebrovascular CO2 reactivity depends on CBF through a sharply nonlinear relationship (see inset in Fig. 4); when CBF falls below an alarm threshold (indicating the initiation of ischemia), CO2 reactivity is suddenly withdrawn. As a consequence of this assumption, cerebrovascular response to hypocapnia progressively disappears when mean SAP decreases below the autoregulation lower limit (SAP < 50 mmHg) in accordance with data by Artru and Colley (2). The existence of an “ischemic threshold” for CBF, below which CO2 reactivity drops to zero, is also confirmed by clinical observations (8).

Interaction Between CBF Control and ICP

The existence of a close relationship among the action of CBF control mechanisms, cerebral blood volume changes, ICP, and intracrani al dynamics is a peculiar characteristic of cerebrovascular regulation that is not shared by other vascular beds. This has been stressed by several authors in past years, beginning with the pioneering works by Lundberg (28), up to the fundamental studies that appeared in the mid-1980s by Rosner and Becker (see e.g., Ref. 42). Using a previous version of the present model (51), we were able to support most of Rosner’s ideas; the model predicted in pathological conditions the generation of self-sustained ICP oscillations very similar to plateau waves. This is a result of a potential positive feedback among autoregulation, CBV changes, and ICP, called by those authors “vasodilatory cascade.”

The new simulation results presented in Figs. 10 and 11 confirm the existence of a similar vasodilatory cascade in response to maneuvers that alter CO2 concentration in blood. Two main aspects of these simulations deserve consideration. First, the impact of CO2 changes on ICP crucially depends on the status of intracranial compensatory mechanisms (CSF outflow and intracranial elastance). The same maneuver, with almost no effect on ICP in physiological conditions, can potentially induce dramatic ICP changes in pathological states characterized by reduced CSF outflow and poor intracranial capacity. In the worst conditions, even a mild hypercapnia can induce a disproportionate transient ICP rise, similar to that of a single plateau wave, with the risk of acute intracranial hypertension and cerebral ischemia (Fig. 10).

Furthermore, the results of Fig. 11 indicate how hyperventilation can be used to control ICP in patients at risk of intracranial hypertension. It should be noted that, in our model, the effect of CO2 changes on ICP depends on two concurrent mechanisms that usually operate with different time constants: 1) active CBV changes, which cause rapid alterations in ICP, generally within a minute of the maneuver; and 2) alteration in CSF production rate, which takes place with a longer time constant (several minutes) and contributes to set the final steady-state ICP level. In the model, CSF production rate depends on capillary pressure and is therefore proportional to CBF.

An important new aspect of this model concerns the relationship between CBF and VmCA. In this study we assumed that the MCA behaves passively, i.e., its inner radius is a monotonic function of transmural pressure; neither autoregulation nor CO2 significantly affects the caliber of the MCA in the model. The consequence of such an assumption is that, during moderate variations in arterial pressure, velocity does not decrease, unlike CBF, due to variations in cross-sectional area. This behavior is supported by the experimental results by Nelson et al. (35) in the rabbit. In contrast, during CO2 alterations, the velocity percent changes are of the same order as CBF changes, because transmural pressure and cross-sectional area in the large arteries remain almost unaffected. This model behavior agrees with data reported previously (30, 44). It is possible, however, that a different behavior for the MCA (inner radius being dependent on PaCO2, or on an active myogenic response) may have significant consequences on model performance.

In perspective, the possibility of simulating the time pattern of ICP and TCD velocity in response to maneuvers affecting CO2 and/or mean SAP could be used to estimate the main parameters of intracranial dynamics from measurements taken in neurosurgical intensive care units. On the basis of knowledge of these parameters in the individual patient, a greater understanding of pathophysiological mechanisms can be achieved and a more well-founded treatment for severe brain damage developed. This model application on real velocity and ICP tracings is the subject of a second, related study (27).
APPENDIX

Quantitative Model Description

Cerebral hemodynamics and CSF dynamics. The fundamental equations describing cerebral hemodynamics are written by imposing volume preservation equations at all nodes of Fig. 1.

Volume balance at the proximal arterial segment (large pial arteries) is

$$G_1(P_a - P_1) - G_{12} \left( \frac{P_1 - P_2}{G_1 + G_2} \right) = \frac{1}{2} \frac{dV_1}{dt}$$ (1A)

where $G_1$ and $G_2$ are the hydraulic conductances of proximal and distal arterial segments, respectively; $P_a$ is mean cerebral arterial pressure assumed equal to SAP; $P_1$ and $P_2$ are the intravascular pressures in the representative sections of large and small pial arteries; and $V_1$ is blood volume contained in the proximal arterial segment.

Volume balance at the distal arterial segment (small pial arteries) is

$$G_1G_2 \left( \frac{P_1 - P_2}{G_1 + G_2} \right) - G_2(P_2 - P_3) = \frac{1}{2} \frac{dV_2}{dt}$$ (2A)

where $P_2$ is intravascular pressure at the representative section of pial arterioles, $V_2$ is blood volume contained in the distal arterial segment, and $P_3$ is cerebral capillary pressure.

Volume balance at the cerebral capillaries is

$$2G_2(P_2 - P_3) - G_{pv}(P_c - P_{pv}) = G_1(P_c - P_{ic}) \cdot H(P_c - P_{ic})$$ (3A)

where $G_{pv}$ is the hydraulic conductance in the proximal segment of cerebral veins, $P_c$ is cerebral venous pressure, $P_{ic}$ is intracranial pressure, and $G_1$ is the conductance to CSF production. It should be noted that the right-hand member of Eq. 3A represents the CSF production rate from cerebral capillaries; we used the Heaviside function $[H(\{\})]$, represented by means of a diode in the electric analog, to indicate that CSF production rate is unidirectional.

Volume balance at the large cerebral veins is

$$G_{pv}(P_c - P_{pv}) - G_{vs}(P_v - P_{vs}) = C_{vi} \left( \frac{dP_v}{dt} - \frac{dP_{ic}}{dt} \right)$$ (4A)

where $G_{vs}$ is the hydraulic conductance of the terminal venous vascular bed, including the lateral lakes and the bridge veins, $P_{vs}$ is sinus venous pressure, and $C_{vi}$ is intracranial venous compliance. The right-hand member of Eq. 4A represents blood volume changes in the venous vascular bed.

Volume balance at the dural sinuses is

$$G_{vs}(P_v - P_{vs}) + C_{ve} \left( \frac{dP_v}{dt} \right) = G_{ve}(P_v - P_{cv}) + C_{ve} \left( \frac{dP_{vs}}{dt} \right)$$ (5A)

where $C_{ve}$ is the conductance to CSF outflow and $G_{ve}$ and $C_{ve}$ are the conductance and compliance, respectively, of the extracranial venous drainage pathways down to the central venous pressure ($P_{cv}$). The second term in the left-hand member of Eq. 5A represents the CSF reabsorption rate at the dural sinuses, which is assumed to be passive and unidirectional. The right-hand member of Eq. 5A denotes blood flow in the extracranial veins.

CONSTANT OF OVERALL CRANIOSPINAL VOLUME (MONRO-KELLIE DOCTRINE). Imposing the balance of the total craniospinal volume, we obtain

$$C_{ic} \left( \frac{dP_{ic}}{dt} \right) = \frac{1}{k_E \cdot P_{ic}} \frac{dP_{ic}}{dt} = \frac{dV_1}{dt} + \frac{dV_2}{dt}$$

$$+ G_1(P_c - P_{ic}) \cdot H(P_c - P_{ic}) + C_{vi} \left( \frac{dP_v}{dt} - \frac{dP_{ic}}{dt} \right)$$ (6A)

where, according to the previous equations, the first five terms in the right-hand member of Eq. 6A represent blood volume changes in the proximal and distal arterial segments, CSF production rate, volume changes in the cerebral veins, and CSF reabsorption rate, respectively. Finally, $I_i$ denotes the amount of artificial CSF injected into (if positive) or subtracted from (if negative) the craniospinal space during clinical maneuvers (PVI tests).

Finally, a value characterizing CBF ($q$) can be computed as the product of conductance and pressure drop in any longitudinal segment (CSF circulation being negligible compared with CBF). By considering the segment of small pial arteries, we have

$$q = 2G_2(P_2 - P_c)$$ (7A)

Biomechanics of arterial-arteriolar cerebral vascular bed. In Eq. 8A, subscript $j$ denotes a quantity belonging to the segment of large pial arteries, whereas subscript $j$ refers to pial arterioles.

The equilibrium of tangential forces in a vessel wall is provided by the Laplace law

$$P_j r_j - P_{pv}(r_j + h_j) = T_{e,j} + T_{m,j} + T_{v,j}$$ (8A)

where $r_j$ is inner radius, $h_j$ is wall thickness, and $T_{e,j}$, $T_{m,j}$, and $T_{v,j}$ represent elastic, smooth muscle (active), and viscous tensions (force per unit length), respectively.

Elastic stress (force per unit surface) increases exponentially with inner radius, reflecting the behavior of elastin and collagen fibers in the wall. Hence we have

$$\sigma_{e,j} = \sigma_{e,0,j} \left[ \exp \left( \frac{r_j - r_{0,j}}{h_{0,j}} \right) - 1 \right] - \sigma_{coll,j}$$ (9A)

$$T_{e,j} = \sigma_{e,j} h_j$$ (10A)

where $\sigma_{e,j}$ is elastic stress, $r_0$ is the inner radius in the condition of "unstressed wall," and $K_{e,j}$, $\sigma_{0,j}$, and $\sigma_{coll}$ are constant parameters. In particular, $\sigma_{coll}$ has been introduced to permit the vessel to sustain a moderate negative tension before collapsing.

Smooth muscle tension depends on inner radius through a campanular relationship, which reflects the different overlapping of actin and myosin filaments. Active tension is therefore maximal at a particular optimal value of inner radius and then progressively decreases. We have

$$T_{m,j} = T_{max,j} \cdot \exp \left[ - \frac{r_j - r_{m,j}}{r_{m,j} r_{m,j}} \right]$$ (11A)

where $r_m$ represents the optimal radius at which smooth muscle exerts its maximal force, $T_{max,j}$ is the corresponding active tension, and $r_{s,j}$ and $n_{m,j}$ are constant parameters used to...
represent the appropriate shape of the campanular relationship.

For the sake of simplicity, we assumed that viscous stress \( \sigma_r \) has a linear dependency on the time derivative of wall strain. Thus

\[
\sigma_{r,j} = \frac{\eta_j}{r_{0,j}} \frac{dr_j}{dt} \quad j = 1, 2 \tag{12A}
\]

\[
T_{r,j} = \sigma_{r,j} h_j \quad j = 1, 2 \tag{13A}
\]

where \( \eta_j \) denotes wall viscosity.

An expression for wall thickness, to be used in Eq. 8A, has been computed by assuming that vessel wall volume remains constant. By neglecting longitudinal strain, we have

\[
h_j = -r_j + \sqrt{r_j^2 + 2r_{0,j} h_{0,j} + h_{0,j}^2} \quad j = 1, 2 \tag{14A}
\]

where \( h_j \) is wall thickness in the unstressed condition (i.e., when \( r = r_{0,j} \)).

Equations 8A–14A provide a value for inner radius in the proximal and distal arterial segments if intravascular and extravascular pressures (\( P_v \) and \( P_e \)) and the optimal smooth muscle tensions (\( T_{max,j} \)) are known. The latter parameter is under the control of regulatory actions (see Cerebrovascular regulation mechanisms). Starting with the radius, approximate expressions for intravascular conductance (\( G_j \)) and blood volume changes (\( dV_j/dt \)) for use in Eqs. 1A–3A, 6A, and 7A can be obtained by mimicking each segment as the parallel arrangement of several vessels with equal diameter. According to the Hagen-Poiseuille law, conductance is proportional to the fourth power of the inner radius

\[
G_j = K_{G,j} r_j^4 \quad j = 1, 2 \tag{15A}
\]

where \( K_G \) is a constant parameter whose value is set to obtain a physiological pressure drop in basal condition. Blood volume, in turn, is proportional to the second power of the inner radius

\[
V_j = K_{V,j} r_j^2 \quad j = 1, 2 \tag{16A}
\]

where a value for the constant parameter \( K_V \) is set to obtain physiological values of blood volume in each segment. By computing the time derivative of Eq. 16A, we obtain

\[
\frac{dV_j}{dt} = 2K_{V,j} \frac{dr_j}{dt} \quad j = 1, 2 \tag{17A}
\]

Biomechanics of cerebral venous circulation. Because the intracranial venous circulation behaves in a passive way (4), we assumed that venous compliance is inversely proportional to transmural pressure. Hence, we have

\[
C_{vi} = \frac{1}{k_{ven}(P_v - P_{ic})} \tag{18A}
\]

where \( k_{ven} \) and \( P_{v1} \) are constant parameters. The latter represents the transmural pressure value (usually slightly negative) at which cerebral veins collapse.

The conductance values for the intracranial veins (\( G_{pv} \) and \( G_{ve} \)) can be computed by assuming that the intracranial venous circulation behaves as a Starling resistor (50), i.e., the conductance of the terminal veins (\( G_{ve} \)) is supposed to depend on pressures through the following relationship

\[
G_{vs} = G_{ve} \left( \frac{P_v - P_{ic}}{P_v - P_{ve}} \right) \tag{19A}
\]

where \( G_{ve} \) is a constant parameter representing the value of conductance when \( P_{ic} = P_{ve} \). Because of the collapse of the terminal vein, cerebral venous pressure is higher than ICP; hence, the large cerebral veins remain open. The conductance \( G_{pv} \) is independent of pressure, that is, a constant value for this parameter has been set throughout the present simulations.

Blood flow velocity in middle cerebral artery. The inner radius of the MCA (\( r_{MCA} \)) is computed as a function of transmural pressure, assuming a monoeponential pressure-radius relationship (20). The \( r_{MCA} \) is therefore a logarithmic function of transmural pressure, \( P_a - P_{ic} \)

\[
r_{MCA} = r_{MCA0} \left( 1 + \frac{P_{ic} - P_{an}}{P_{ic} - P_{an}} \right) \tag{20A}
\]

where \( K_{MCA} \) is a constant parameter and \( r_{MCA0} \) denotes the inner radius in basal condition.

Finally, blood velocity (\( V_{MCA} \)) is computed as the ratio of blood flow and cross-sectional area, assuming that about one-third of total CBF passes through each MCA. Hence

\[
V_{MCA} = \frac{q}{\pi (\frac{1}{3} r_{MCA}^2)} \tag{21A}
\]

Cerebrovascular regulation mechanisms. Cerebrovascular control mechanisms affect smooth muscle tension in pial arteries by modifying the amplitude of the active tension relationship (i.e., \( T_{max} \) in Eq. 11A). We have

\[
T_{max,j} = T_{max,0,j} (1 + M_j) \quad j = 1, 2 \tag{22A}
\]

where \( T_{max} \) is the optimal smooth muscle tension in basal condition and \( M \) is an activation factor that accounts for the degree of smooth muscle contraction or dilation. In basal conditions \( M = 0 \). Furthermore, \( 1 < M < 0 \) indicates vasodilation, whereas \( 0 < M < 1 \) represents vasoconstriction.

The activation factor is the result of two contributions, \( x_{aut} \) and \( x_{CO_2} \), which account for the effect of autoregulation and \( CO_2 \) reactivity, respectively. Both are state variables, the dynamics of which have been assumed to be of the first order (see below).

CEREBRAL AUTOREGULATION. In accordance with physiological literature, we assumed that autoregulation acts on large pial arteries and pial arterioles through two distinct feedback mechanisms. Smooth muscle tension in the proximal segment depends on perfusion pressure changes. Hence, the following differential equation holds for the variable \( x_{aut} \)

\[
\tau_{aut,1} \frac{dx_{aut,1}}{dt} = -x_{aut,1} + G_{aut,1}(P_a - P_v - P_{an} + P_{vn}) \tag{23A}
\]

where \( G_{aut,1} \) and \( \tau_{aut,1} \) are the mechanism gain and time constant and \( P_{an} - P_{vn} \) is normal CPP. According to Eq. 23A, any decrease in CPP causes a vasodilation in large pial arteries, whereas a perfusion pressure increase causes vasoconstriction.

In the small pial arteries (second segment in Fig. 1), we assumed that autoregulation is triggered by changes in CBF. Accordingly, the quantity \( x_{aut,2} \) is governed by the following differential equation

\[
\tau_{aut,2} \frac{dx_{aut,2}}{dt} = -x_{aut,2} + G_{aut,2} \left( \frac{q - q_1}{q_1} \right) \tag{24A}
\]

where, as in Eq. 23A, \( G_{aut,2} \) and \( \tau_{aut,2} \) are gain and time constants, and the parameter \( q_1 \) represents the value of CBF that satisfies the metabolic need (and so does not activate the
CO₂ REACTIVITY. Because CO₂ acts mainly through changes in the pH of the perivascular space, we assumed that the state variables xCO₂\textsubscript{j} (j = 1, 2) depend on the logarithm of CO₂ pressure in arterial blood. Moreover, the nature of CO₂ reactivity does not differ substantially in large and small pial arteries. The following differential equations can thus be written

\[
\tau_{CO₂} \frac{d(x_{CO₂,j})}{dt} = -x_{CO₂,j} - G_{CO₂,j} \frac{A_{CO₂} \log_{10} \left( \frac{P_{ACO₂}}{P_{ACO₂,n}} \right)}{4} \quad (25A)
\]

where \( G_{CO₂,j} \) and \( \tau_{CO₂} \) denote the mechanism gain and time constant and the subscript n is used to represent the \( P_{ACO₂} \) value that does not affect the basal smooth muscle tension. According to Eq. 25A, hypercapnia causes vasodilation in both pial segments, whereas hypocapnia causes vasoconstriction. Finally, in accordance with the corrective factor \( A_{CO₂} \), we assumed that the strength of the CO₂ regulation mechanism remains quite constant when CBF is normal or moderately decreased but rapidly drops to zero during severe ischemia. We used the following dependence of \( A_{CO₂} \) on CBF

\[
A_{CO₂} = \frac{1}{1 + \exp \left[ -K_{CO₂}(q - q_n)/q_n - b_{CO₂} \right]} \quad (26A)
\]

where \( K_{CO₂} \) and \( b_{CO₂} \) are constant parameters. These parameters were set so that \( A_{CO₂} \) remains almost 1 until CBF is greater than 50% of \( q_n \), and then exponentially decreases (see inset in Fig. 4). As a consequence, the CO₂ reactivity of pial vessels vanishes during severe ischemia.

INTERACTION BETWEEN AUTOREGULATION AND CO₂ REACTIVITY. The two state variables \( x_{aut} \) and \( x_{CO₂} \) interact in a nonlinear way through a sigmoidal relationship, yielding the activation factor \( M \). We therefore have

\[
M_j = \frac{M_{min,j} + M_{max,j} \exp \left[ (x_{aut,j} + x_{CO₂,j})/K_{M,j} \right]}{1 + \exp \left[ (x_{aut,j} + x_{CO₂,j})/K_{M,j} \right]} \quad (27A)
\]

where \( M_{min} \) and \( M_{max} \) are the lower and upper saturation levels of the sigmoidal relationship, representing the limits for smooth muscle tension, and \( K_{M} \) is a constant parameter that permits setting of the central slope (i.e., the slope when \( x_{aut} + x_{CO₂} = 0 \)). In this model we assumed that the central slope is always equal to 1. This is achieved by assuming \( K_{M,j} = M_{max,j} - M_{min,j}/4 \). Because of this assumption, each mechanism acting individually is equal to \( G_{aut} \) and \( G_{CO₂} \) in Eqs. 23A–25A.

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